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Prediction of Faults using Hydrocarbon Gases Data of Mineral Oil Immersed Power Transformers using Computer Intelligence



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Introduction

Dissolved Gas Analysis has been used extensively for more than 40 years. It is a very efficient tool for the early diagnosis of fault assurance and increases the opportunity for precautionary measure. Most of the Electrical facilities in South India were commissioned in the late 1950s .FIG.1.shows the Distribution Growth 1957 since in of TNEB1.In TamilNadu[website certain Substations and Distribution areas, the Electrical Switch Gear and Systems are more than 50 years of age. Depending upon the usage of the Equipment and Environmental conditions, they may be at the nearer end of their useful lives. Transformers are some of the most efficient Electrical Machines with some large units able to transfer 99.75% of their input power to their output. In larger Transformers part of the problem is removal of heat. Mineral oils are used for insulation and the windings immersed in this oil transfer heat to the oil thereby getting cooled. The oils are the mixture of many different Hydrocarbon Molecules which decompose under high Thermal and Electrical Stress within the transformer during the period of service .The critical changes are the breaking of Carbon-Hydrogen and Carbon-Carbon bonds as a result of which different gases are formed due to the presence of individual Hydrocarbon and the distribution of Energy and the Temperature in the neighbourhood of the fault. The causes of fault gases can be divided into three categories [Joseph **B.DiGiorgio**].

a)Corona or Partial Discharge

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Abstract

This work proposes the separation of Faults diagnosed from Hydrocarbon Gas Data Collected from Dissolved Gas Analysis of Power Transformers over a period of a Decade in the area of Tirunelveli District in South India. The condition of Power Transformers is diagnosed using Fuzzy Set Theory. (FST) Simulations are compared with conventional methods. The computational Efficiency ,Reliability and Success are evaluated and compared. FST is found to be more reliable ,efficient and its success rate is also high.

b)Pyrolysis or Thermal Heating c)Arcing

These three categories differ mainly in the intensity of energy that is dissipated per unit time per unit volume by the fault. The most severe intensity of energy dissipation occurs at Arcing, less with Heating and least with Corona.

The fault gases that can be found in a unit are Hydrocarbons like HydrogenH₂, Methane CH₄, Ethane C₂H₆, Ethylene C₂H₄, Acetylene C₂H₂ and carbon oxides such as CO,CO₂ in addition to no-fault gases like N₂ and O₂. The majority of gases that are found indicative of faults are also those that are more soluble in Oil. At a pressure of 760 mm Hg and 25° C temperature, the solubility of gases in Transformer oil is found to be as shown in Table 1.

| Table | 1. | Solu | bility | Of | Gases |
|-------|----|------|--------|----|-------|
|-------|----|------|--------|----|-------|

| H_2 | 7 % by volume |
|----------------|-----------------|
| N ₂ | 8.6 % by volume |
| CO | 9.0 % by volume |
| O ₂ | 16 % by volume |
| CH_4 | 30 % by volume |
| CO_2 | 120 % by volume |
| C_2H_6 | 280 % by volume |
| C_2H_4 | 280 % by volume |
| C_2H_2 | 400 % by volume |



Fig.1.Distribution Growth Since 1957

Over a temperature range 0 to 80 degree Centigrade some gases increase in solubility upto 79 % while others decrease their solubility up to 66 %.[Wan, Yat How and Marzuki Khalid (1999).] .By extracting the dissolved gases in the oil, they are separated ,identified and quantitatively determined by DGA method.Eventhough the data from DGA is found to be inconsistent ,since it detects the gases in the oil phase giving the earliest possible detection of an incipient fault, the DGA technique is a very efficient tool.

Thermal Faults

The decomposition of mineral oil (from 150° C to 500° C) produces relatively large quantities of the low molecular weight gases, such as H₂,CH₄ and trace quantities of the higher molecular weight gases Ethylene (C_2H_4) and Ethane (C_2H_6) . As the fault temperature in mineral oil increases to modest temperatures, the Hydrogen concentration exceeds that of Methane ,but now the temperatures are accompanied by significant quantities of higher molecular weight gases -First Ethane and then Ethylene .At the upper of the Thermal Fault Range, increasing quantities Hydrogen and Ethylene and of Acetvlene traces $(C_{2}H_{2})$ mav be produced.[IEEE standards C57.104 TM-(2008)]. The presence of Acetylene suggests a high temperature fault, perhaps an arc has occurred in the oil in a Transformer, the presence of Methane suggests that - if a fault has occurred- it is a lower energy electrical or thermal fault.

Electrical Faults

a)Low Intensity Discharges: Produce mainly Hydrogen with decreasing quantities of Methane and trace quantities of Acetylene.As the intensity of discharge increases ,the Acetylene, and Ethylene concentrations rise significantly.

b)High Intensity Arcing: As the intensity of Electrical Discharge reaches Arcing or continuing Discharge proportions that produce temperatures from 700° C to 1800° C, the quantity of Acetylene becomes pronounced.

Probability of Transformer Failure

In this work Evaluation of possible types of faults is carried out by analysis of separate combustible HydroCarbon Gases. The method used for the analysis using simulink in MATLAB is the Rogers Ratio Method[**R.R.Rogers(1978**)]. The total volume of evolved gas is an indicator of the magnitude of incipient

faults.To determine the volume, in gallons, of Total Dissolved Gases Combustible in insulating oil (TDGCv) the following Equation is used.[IEEE standards C57.104 TM-(2008)].

TDGCv=FG(V)/1000000;Where FG (Fault Gases) is the sum of H₂, CH₄, C₂H₆, C₂H₄, C₂H₂ and C [micro litres/litre] V is the volume of oil in transformer [litres (gallons)] TDCGv is the total dissolved combustible gas volume [litres (gallons)]

This straight forward method is useful for completely oil-filled (conservator type) transformers with conditions that produce small quantities of fault gas. These conditions warrant continuous monitoring; this fault case volume method continues to be useful as fault conditions enlarge, with the added advantage that it permits continuous monitoring of insulation deterioration in spite of any oil handling activity that includes degasification.

Diagnosis

The diagnostic theories based upon the thermal degradation principles employ an array of ratios of certain key combustible gasses as the fault type indicators. These five ratios are [**Dr.Joseph B.DiGiorgio and, Wan, Yat How and Marzuki Khalid (1999)**]

Ratio 1 (R1) = CH_4/H_2 Ratio 2 (R2) = C_2H_2/C_2H_4 Ratio 3 (R3) = C_2H_2/CH_4 Ratio 4 (R4) = C_2H_6/C_2H_2 Ratio 5 (R5) = C_2H_4/C_2H_6

The Rogers method utilizes ratios 1,2 and 5. The Roger's method does not depend on specific gas concentration to exist in the transformer for the diagnosis to be valid but the Doernenburg **[IEEE standards C57.104 TM-(2008)]**ratio utilizes ratios 1,2,3 and 4and requires significant levels of gases to be present in order for the diagnosis to be valid. . However Rogers suggests that the method be used only when the normal limits of individual gases(refer Table 2) have been exceeded.

A four level criterion has been developed to classify risks to transform as when there is no previous dissolved gas history, for continued operation at various combustible gas levels. The criterion uses both concentrations for separate gases and the total concentration of all combustible gases.[IEEE standards C57.104 TM-(2008)].

| Table-2 Limit Concentrations Of Dissolved Ga | Table-2 | f Dissolved Ga | Concentrations (| Gas |
|----------------------------------------------|---------|----------------|-------------------------|-----|
|----------------------------------------------|---------|----------------|-------------------------|-----|

| Key gas | Concentrations L | | | | | |
|-------------------------------------------|---------------------------|--|--|--|--|--|
| | (Micro litres/litre(ppm)) | | | | | |
| Hydrogen(H ₂) | 100 | | | | | |
| Methane(CH ₄) | 120 | | | | | |
| Carbon Monoxide(CO) | 350 | | | | | |
| Acetylene(C ₂ H ₂) | 1 | | | | | |
| Ethylene(C_2H_4) | 50 | | | | | |
| Ethane(C_2H_6) | 65 | | | | | |

Condition 1 : TDCG below this level indicates the transformer is operating satisfactorily. Any individual combustible gas exceeding specified levels should prompt additional investigation.

Condition 2 : TDCG within this range indicates greater than normal combustible gas level. Any individual combustible gas exceeding specified levels should prompt additional investigation. Action should be taken to establish a trend.Faults may be present.

Condition 3 : TDCG within this range indicates a high level of decomposition Any individual combustible gas exceeding specified levels should prompt additional investigation.Immediate action should be taken to establish a trend .Faults are probably present.

Table 3- Dissolved Key Gas Concentrations

Condition 4 : TDCG exceeding this value indicates excessive decomposition .Continued operation could result in failure of the transformer. Proceed immediately with caution. The Dissolved key gas concentration limits (ppm) for each condition is shown in Table 3.

Evaluation of possible type of fault by the Rogers ratio method:

The Rogers ratio method uses only three ratios(R1,R2,R5). This method is also based on the thermal degradation principle. Table 4 gives the values for the three key gas ratios corresponding to suggested diagnoses. These ratios according to Rogers are applicable to both gases taken from the gas space and gases extracted from the oil. The fault types given in Table 4 have been chosen from the fault types originally suggested by Rogers.

Fuzzy Rogers Ratio System

Fuzzy Rogers Ratio system uses the 5 fault gases which are Acetylene, Ethylene, Methane, Hydrogen and Ethane to determine 9 transformer conditions. Therefore, the structure for the Fuzzy Rogers Ratio system can be illustrated as in **Figure 3** where the ratios are identified as the input parameters while the 9 interpretation results based on the different combination of ratios are identified as the output parameter as listed below.

The test results of DGA for data collected from Electricity Board are tabulated below for a few random samples. The remarks predicts suspected occurrence of Thermal Fault above 100^oC due to Overheating. Out of the 551 samples collected from various Transformers located at different substations 329 samples are no fault data and 137 are recommended resampling by the TNEB Test Lab. These 137 samples were tested with Rogers Ratio Simulink and Fuzzy Rogers Ratio System and the results are compared.

| Status | Dissolved Key gas concentration limits [µL/L(ppm)] | | | | | | | | | |
|------------|----------------------------------------------------|-------------------------------|----------------------------------|----------------------------------|----------------------------------|--------------------|--------------------|-------------------|--|--|
| | Hydrogen | Methane (CH ₄) | Acetylene | Ethylene | Ethane | Carbon Monoxide | Carbon Dioxide | TDCG ^a | | |
| | (H ₂) | (0114) | (C ₂ H ₂) | (C ₂ H ₄) | (C ₂ H ₆) | (CO) | (CO ₂) | | | |
| Condition1 | 100 | 120 | 1 | 50 | 65 | 350 | 2500 | 720 | | |
| Condition2 | 101-700 | 121-400 | 2-9 | 51-100 | 66-100 | 351-570 | 2500-4000 | 721-120 | | |
| Condition3 | 701-1800 | 401-1000 | 10-35 | 101-200 | 101-150 | 571-1400 | 4001-10000 | 1921-4630 | | |
| Condition4 | >1800 | >1000 | >35 | >200 | >150 | >1400 | >10000 | >4630 | | |

^aTDCG value does not include CO₂, which is not a combustible gas.

| Case | R2 | R1 | R5 | Suggested fault diagnosis |
|------|------------|--------------|------------|---------------------------------|
| | C2H2/C2H4 | CH4/H2 | C2H4/C2H6 | ungnosis |
| 0 | <0.1 | >0.1 to <1.0 | <1.0 | Unit normal |
| 1 | <0.1 | <0.1 | <1.0 | Low energy density arcing-PD |
| 2 | 0.1 to 3.0 | 0.1 to 1.0 | >3.0 | Arcing-High energy discharge |
| 3 | <0.1 | >0.1 to <1.0 | 1.0 to 3.0 | Low temperature thermal |
| 4 | <0.1 | >1.0 | 1.0 to 3.0 | Thermal<700deg |
| 5 | <0.1 | >1.0 | >3.0 | Thermal>700deg |

Table 4-Rogers Ratio For Key Gases

Rogers Simulink Model in MATLAB is shown in Fig.2.

| Fault | Fault Type | Ranges of gas ratio | | | | | |
|-------|-------------------------------------|---------------------|---------------------------------|-----------------|--|--|--|
| code | | C_2H_2/C_2H_4 | CH ₄ /H ₂ | C_2H_4/C_2H_6 | | | |
| 0 | No fault | < 0.1 | 0.1-1.0 | <1.0 | | | |
| 1 | Low energy partial discharges | <0.1 | < 0.1 | <1.0 | | | |
| 2 | High energy partial discharges | 0.1-3 | < 0.1 | <1.0 | | | |
| 3 | Low energy discharges | >0.1 | 0.1-1.0 | >1.0 | | | |
| 4 | High energy discharges | 0.1-3 | 0.1-1.0 | >3.0 | | | |
| 5 | Low temperature fault 150°C | <0.1 | 0.1-1.0 | 1.0-3.0 | | | |
| 6 | Low temperature fault 150- 300°C | <0.1 | >0.1 | <1.0 | | | |
| 7 | Medium temperature fault 300-700°C | <0.1 | >0.1 | 1.0-3.0 | | | |
| 8 | High temperature fault>700°C | <0.1 | >0.1 | >3.0 | | | |

The Ratios are fuzzified[Zimmerman,H.J. (1986) and R.Naresh,Veena Sharma Vashisth, and Manisha (2008]using the following Linguistic variables and membership functions as shown below.



Methane

Ethane

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FIG.6 SAMPLE TEST OUTPUT FOR R1=1.16; R2=1.06; R5=1.77

TABLE-5 HYDROCARBON GASES FROM DGA DATA-Date of Commissioning 08.11.2005

| HC Values in ppm | H_2 | CH_4 | C_2H_6 | C_2H_4 | C_2H_2 | CO_2 | CO | Remarks |
|-----------------------|-------|--------|----------|----------|----------|--------|----|-------------------------------------------|
| 16 MVA,110/11kV | | | | | | | | By Lab Expert |
| Sample I-03.01.2006 | 46 | 168 | 37 | 286 | 2 | 840 | - | |
| Sample II-17.01.2006 | 64 | 224 | 49 | 376 | 2 | 1164 | - | Thermal Fault of above 100 ⁰ C |
| Sample III-06.02.2006 | 38 | 219 | 52 | 377 | 1 | 1340 | - | Due to Overheating |
| Sample IV-16.03.2006 | 29 | 189 | 75 | 353 | 2 | 1454 | - | |
| Sample V-11.04.2008 | 14 | 67 | 42 | 111 | 0 | 1223 | - | Resample |
| Sample VI-07.08.2008 | 22 | 94 | 43 | 138 | 3 | 1823 | - | |
| SampleVII-27.04.2009 | 25 | 96 | 50 | 158 | 6 | 1964 | - | Satisfactory |

IV.RESULTS

TABLE-6 RESULTS

| Conventional Rogers Ratio | | | Fuzzy Rogers Ratio System | | | | |
|---------------------------|-----|-----|---------------------------|----|-----|--|--|
| Simulink Mod | lel | | | | | | |
| Samples taker | ı: | 137 | Samples taker | 1: | 137 | | |
| Consistent | : | 83 | Consistent | : | 95 | | |
| Inconsistent | : | 54 | Inconsistent | : | 42 | | |
| Success | : | 64 | Success | : | 87 | | |
| Failure | : | 19 | Failure | : | 08 | | |
| % of Success | : | 80 | % of Success | : | 91 | | |
| Efficiency | : | 77 | Efficiency | : | 92 | | |

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Rogers Ratio Code

Transformer Faults

FIG.3 FUZZY ROGERS RATIO SYSTEM



FIG .2. ROGERS SIMULINK MODEL IN MATLAB

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