

## Journal of Asian Scientific Research

journal homepage: http://aessweb.com/journal-detail.php?id=5003

# TUNED SIMULATED ANNEALING BASED ON BOLTZMANN AND BOSE-EINSTEIN DISTRIBUTION APPLIED TO MAXSAT PROBLEM

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# ABSTRACT

In this paper, a hybrid Simulated Annealing algorithm using Boltzmann and Bose-Einstein Distributions (SABBE) is proposed. SABBE was designed for solving satisfiability (SAT) instances, and it has three phases: i) BP (Boltzmann Phase), ii) BEP (Bose-Einstein Phase), and iii) DEP (Dynamical Equilibrium Phase). BP and BEP are simulated annealing searching procedures based on Boltzmann and Bose-Einstein distributions respectively. BP ranges from high to low temperature values, while BEP goes from low to very low temperatures. Another simulated annealing search procedure, DEP, is applied at the final temperature of the second phase. However, DEP uses a particular heuristic for detection of stochastic equilibrium by employing a least squares method during its execution. Finally, SABBE parameters are tuned with an analytical method, which considers the maximal and minimal deterioration of SAT instances.

Keywords: C630 - Computational techniques, Simulated annealing, Heuristic algorithms.

# **1. INTRODUCTION**

Satifiability problem (SAT) plays a significant role in combinatorial optimization and computational complexity theory. It is well known that SAT is NP-Complete [1], and any instance of an NP problem may be converted to a SAT instance. Thus, any efficient algorithm for SAT problem might be used for solving other NP-Complete problems. In this paper, a particular SAT problem known as Max Sat is boarded. The goal of Max Sat is to maximize the number of clauses of a boolean formula. Satisfiability problem consists in finding a truth assignment such that it satisfies a well formed arbitrary boolean expression [2]. Usually, any SAT instance is in the Conjunctive Normal Form (CNF). A SAT (or Max SAT) instance is defined as follows: a) a set of m clauses:  $C_1, C_2, ..., C_m$ , b) a set of n variables  $x_1, x_2, ..., x_n$ , and c) a set of literals, where a literal is a variable or a negation of it. Max SAT can be solved by several efficient algorithms as Simulated Annealing (SA) [3, 4], Genetic Algorithms [5, 6], Neural Networks [7], Spears [8] Guided Local Search [9], Swarm optimization [10], Extreme optimization [11, 12], and so on. SA has shown to be very efficient for solving combinatorial optimization problems, specifically the SAT problem.

SA is a heuristic algorithm, which has shown a high performance solving SAT instances in a reasonable processing time [13].

In order to obtain high quality solutions efficiently, our approach tunes SA parameters using an analytical method [14] for determining system temperature and the length of the Markov Chain of the Metropolis Cycle (MC). This technique establishes the temperature values based on maximum and minimum deterioration of a SAT instance. In order to enhance exploration process of the solution space and avoid local optima, Boltzmann and Bose-Einstein distribution are applied by the SABBE algorithm. Boltzmann distribution is used at high temperatures, and Bose-Einstein distribution is used at low temperatures. As a means to reduce system temperature, two different cooling schemes are employed.

This paper is organized as follows: Section 2 describes the classic Simulated Annealing algorithm. Section 3 explains the analytical tuning method, and section 4 introduces SABBE algorithm. Finally section 5 presents the experimental results, and paper conclusions are explained in section 6.

### 2. SIMULATED ANNEALING ALGORITHM

In this section, classical Simulated Annealing is briefly described; we discuss how this algorithm uses the Boltzmann distribution in order to accept poor quality solutions and escape from local optima. Later, Bose-Einstein distribution is described, and the new algorithm based on Boltzmann and Bose-Einstein distribution is introduced

### 2.1. Classical Simulated Annealing

Simulated Annealing (SA) algorithm based on Boltzmann Distribution was introduced in the combinatorial optimization area by Kirkpatrick [15], and Cerny [16]. Boltzmann distribution is fundamental for statistical mechanics, and it is defined by the assumption that all particles are distinguishable, and all possible energy divisions occur with the same probability. Simulated Annealing can find optimal or near-optimal solutions of a specific combinatorial optimization problem. SA randomly explores the solution space of a specific instance, while an objective function is maximizing (or minimizing). Therefore, SA is an approximation algorithm for finding the global optimum. For the MaxSAT problem, the ideal solution is obtained when all clauses are satisfied. SA approach always accepts better solutions. However, when a new solution does not improve the previous one, it is accepted or rejected in accordance to the Boltzmann distribution (1). This function is related to the difference of energy between two solutions ( $S_i$  and,  $S_j$ ), and the current temperature value.

$$P(\Delta E) = e^{-(s_i - s_j)/T} \tag{1}$$

Where  $P(\Delta E)$  is the solution probability acceptance,  $\Delta E$  is the energy difference between S<sub>i</sub> and S<sub>j</sub> solutions, and T is the current temperature value. SA is composed by two cycles: The external cycle which diminish the temperature, and the internal Metropolis Cycle (MC) which explores solution neighborhood by using a distribution function in accordance to the current system temperature. Boltzmann distribution function is applied in MC to examine the space of solutions in a neighborhood for a given temperature. According to the classical thermodynamics properties at high temperatures the probability to change between two energy states is very high. Therefore, the probability of accepting bad solutions at very high temperatures can be taken as number close to one. However, as the system is cooled, this probability decreases towards zero.

### 2.2. Simulated Annealing Based on Bose-Einstein Distribution

Statistical mechanics consists of a set of methods to analyze the properties of large numbers of atoms in the physical environment. The systems modeled by these mechanics contain very large quantities of atoms, therefore only the most probable behavior of the system in thermal equilibrium at a given temperature is observed [17]. In classical physics particles obey Maxwell-Boltzmann distribution; nevertheless quantum particles, like Bosons and fermions, are expressed by a different behavior. While bosons tend to overlap at the same energy level following a Bose-Einstein distribution, only one fermion can occupy an energetic state. If we compare bosons with classical particles at very high temperatures or a high density system, Bose-Einstein becomes Maxwell-Boltzmann statistics. Nevertheless at low temperatures, bosons behave differently from other particles and tend to congregate at the same lowest-energy state, the result is known as a Bose-*Einstein condensate* [18]. Thus, bosons and classical particles behavior is totally different at low temperatures. Therefore, the hypothesis explored in this paper is that Simulated Annealing Algorithm applying both Boltzmann and Bose-Einstein distributions for accepting bad solutions for high and low temperatures will enhance SABBE performance (promoting a fast quality convergence at low temperatures) over the classical Simulated Annealing based exclusively on Boltzmann distribution. Bose-Einstein distribution is given by equation (2).

$$h(\Delta E) = \frac{1}{\left(e^{\lambda}e^{(\Delta E/KT)} - 1\right)}$$
(2)

Where T is the temperature parameter,  $\lambda$  is the total bosons in the system and k is the Boltzmann's constant. Notice that (2) becomes Boltzmann distribution when  $e^{\lambda}$  is equal to one. The use of this distribution as acceptance criteria is detailed in section 3.

### **3. ANALYTICAL TUNING METHOD**

In this section, we firstly describe the tuning method used in this paper. Secondly, the process to determine the length of the Markov chain is shown.

#### **3.1 Setting Initial and Final Temperatures**

The parameters of SABBE are tuned by an analytical method [13, 14, 19]. This computation is based on the deterioration (maximal and minimal) of the SAT instances, and the acceptance probability of solutions. As mentioned before, probability for accepting any new solution is close to one at high temperatures; consequently, the cost function deterioration is maximal. Thus, the initial temperature  $T_0$  is associated with the maximal deterioration  $\Delta Z_{max}$ . On the other hand, the probability for accepting any new solution is close to zero at low temperatures; in this case, the cost function deterioration is minimal. Therefore, the final temperature  $T_f$  is related to the minimal deterioration  $\Delta Z_{min}$ . The acceptance probability based on Boltzmann distribution is defined by (3). At extremely high or low temperatures, this equation leads respectively to equation (4) and (5). The later equation is used to determine the final temperature at the end of the process.

$$P(\Delta Z) = \exp\left(\frac{-\Delta Z}{T}\right)$$

$$T_0 = \frac{-\Delta Z_{\text{max}}}{1 - T - T}$$
(3)
(4)

$$\ln(P(\Delta Z_{\max}))$$

$$T_{i} = \frac{-\Delta Z_{\min}}{2}$$

$$(4)$$

$$I_f = \frac{1}{\ln(P(\Delta Z_{\min}))}$$
(5)

In a similar way, as the system is cooled, initial and final temperatures are obtained by applying Bose-Einstein distribution (see equation 6). Equations (7) and (8) are obtained from equation (6) using the maximum and minimum energy deterioration. SABBE starts its Boltzmann Phase (BP) with the initial temperature defined by equation (4); BP is stopped at the initial temperature defined by equation (7). Once PB finishes, BEP starts. This second phase stops in accordance to the temperature defined by equation (8) which corresponds to the stochastic equilibrium. After BEP finishes, DEP starts using Bose-Einstein distribution dynamically detecting the equilibrium of the process.

$$P(\Delta Z) = \left(\exp\left(\frac{-\Delta Z}{T}\right) - 1\right)^{-1}$$
(6)

$$T_{0} = \frac{\Delta Z_{\text{max}}}{\ln\left(\frac{(P(\Delta Z_{\text{max}}) + 1)}{P(\Delta Z_{\text{max}})}\right)}$$
(7)

$$T_{f} = \frac{\Delta Z_{\min}}{\ln\left(\frac{(P(\Delta Z_{\min}) + 1)}{P(\Delta Z_{\min})}\right)}$$
(8)

#### 3.2 Setting the Markov Chain Length

In SABBE, the length of the Markov Chain (MC) is defined by the number of iterations into the Metropolis Loop (ML), and can be modeled as constant or variable. In constant MC, any ML has the same length; in contrast, when MC is variable, the length of each ML may be different during SABBE execution. Let  $L_k$  be the chain size given a *k* temperature for a ML. In classical SA implementation, ML stops when a specific number of accepted solutions is reached. In contrast, the analytical method determines  $L_k$  with a simple Markov model [14]; at high temperatures, only a few iterations are required due stochastic equilibrium is rapidly reached. Nevertheless, at low temperatures a more exhaustive exploration is required; as consequence, a larger  $L_k$  is used by this analytical method. In the present paper,  $L_k$  is modeled by using equation (9).

$$L_{k+1} = \beta L_{K} \tag{9}$$

Where  $\beta$  represents the increase factor of MC.  $\beta$  is calculated by (10).

$$\beta = \exp\left(\frac{\ln(L_{\max}) - \ln(L_0)}{n}\right) \tag{10}$$

Let  $L_1$  be  $L_k$  at  $T_0$ ,  $L_{max}$  be the maximum MC length, and n is the number of times that the temperature will be decreased during the algorithm. System temperature is reduced using a cooling scheme, such as, (11) or (12).

$$T_{K+1} = \alpha T_k \quad k = 0, 1, ...; \quad 0.7 \le \alpha < 1$$
 (11)

$$T_{K+1} = e^{-\alpha} T_k \quad k = 0, 1, ...; \quad 0.7 \le \alpha < 1$$
 (12)

Whether cooling function (11) is applied, n is calculated by equation (13). Thus, if cooling function (12) is used, n is obtained by equation (14).

$$n = \frac{\ln(T_f) - \ln(T_0)}{\ln(\alpha)} \tag{13}$$

$$n = \frac{\ln(T_f) - \ln(T_0)}{\alpha} \tag{14}$$

### **4. SABBE ALGORITHM**

As mentioned before, SABBE is a hybrid algorithm which has three phases (see Figure 1): i) Boltzmann Phase (BP) from high to low temperatures, ii) Bose-Einstein Phase (BEP) from low to very low temperatures, and iii) Dynamical Equilibrium Phase (DEP). For accepting bad solutions, BP and BEP apply Boltzmann and Bose-Einstein distributions respectively. This is performed in order to escape from local optima. DEP is a kind of BEP extension, where the stochastic equilibrium is detected in a dynamical way. This is done by using a regression method into the metropolis cycle; the number of iterations is considered as the independent variable, while each energy value represents the dependent variable. The criteria used to find equilibrium is the slope of the energy function of the metropolis cycle. Figure 2 shows the BP pseudo code. During each phase depicted in figure 1, better solutions are always accepted. On the other hand, worse solutions are accepted or rejected in accordance to an acceptance function. The length of the Markov chain (i.e. the internal cycle length) for each MC is determined by equation (9), where the increment factor  $\beta$ is calculated by equation (10). In Figure 3, BEP and DEP pseudo code are shown. In BEP, the external cycle decreases temperature accordingly to cooling function (11) or (12). The metropolis cycle length is constant and equal to the maximum length of last metropolis cycle of BP.





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Fig- 2.BP pseudo code.
```

```
BP()
Begin
T = value calculated by equation (4)
n = value calculated by equation(13) or(14)
S<sub>i</sub> = Create_initial_solution()
i = 1
While (i < n) do
k = 1
while (k<=CM) do</pre>
```

For practical reasons DEP is considered as a third phase. DEP goal is to detect system energy equilibrium by analyzing the energy slope between two solutions in accordance to an objective function. Let define  $x_i$  as the iteration number for the metropolis cycle (1, 2,..., n), and  $E_i$  as the current energy (number of satisfied clauses) found by the algorithm in iteration  $x_i$ . Using a standard least squares method, the slope for n iterations is defined by equation (15).

$$m = \frac{n \sum_{i=1}^{n} x_i E_i - \left(\sum_{i=1}^{n} x_i\right) \left(\sum_{i=1}^{n} E_i\right)}{n \sum_{i=1}^{n} x_i^2 - \left(\sum_{i=1}^{n} x_i\right)^2}$$
(15)

The former formula becomes

$$m = K_1 \sum_{i=1}^{n} iE_i - K_2 \sum_{i=1}^{n} E_i \quad where \quad K_1 = \frac{12}{n^3 - n}; K_2 = \frac{6}{n^2 + n}$$
(16)

Notice that the complexity of computing equation (16) is O(n) because both of the summations are computed using a simple data structure (as is shown in Fig. 3), and  $K_1$  and  $K_2$  are only constants for a particular n value.

8	
BEP()	DEP()
Begin	Begin
T = equation (7)	While (m≈0)do
Tfinal = equation (8)	n = 1
While $(T > Tfinal) do$	while $(k \le CM)$ do
k = 1	$Sj = perturbate\_system(S_i)$
while $(k \le CM)$ do	If $E(S_i)$ =total_clausule then stop()
$S_i = perturbate\_system(S_i)$	$\Delta E = E_i - E_i$
If $E(S_i) = total \ clausule \ then \ stop()$	If $(\Delta E \ge 0)$ then

Fig-3. BEP/DEP Pseudo code.

$\Delta E = E_j - E_i$	$S_i = S_i$
If $(\Delta E \ge 0)$ then	$Elself((1/(exp(\Delta E/T)-1))[0,1])$ then
$S_i = S_i$	$S_i = S_j$
Elself $((1/(exp(\Delta E/T)-1))[0,1])$ then	End if
$S_i = S_j$	n = n + 1
End if	$\sum iE = \sum iE + n * Ei$
K = k + 1	$\Sigma E = \Sigma E + Ei$
end while	end while
$T = \alpha * T \text{ or } T = e \cdot \alpha * T$	$T = \alpha * T \text{ or } T = e - \alpha * T$
End while	$k1 = 12/(n^3 - n)$
End	$k2=6/(n^{2}+n)$
	End while
	End

# 5. EXPERIMENTAL RESULTS & DISCUSSION

SABBE algorithm was tested with 36 SAT instances taken from the 2009 SAT competition<sup>1</sup> which are shown in Table 1. These instances are grouped by their  $\rho$  value (number of clauses/number of variables) between 2.07 to 4.25. The temperature ranges for Boltzmann and Bose-Einstein Phases were calculated by applying equations (4), (5), (7), and (8). Table 2 shows the values for T<sub>0</sub> for Boltzmann Phase, as well as T<sub>0</sub> and T<sub>f</sub> for Bose-Einstein Phase. Observe that T<sub>f</sub> for all instances is equal to 0.68 with the minimum deterioration equal to one; P( $\Delta Z_{min}$ ) was taken as 0.3. Table 3 shows n and  $\beta$  parameters for these instances. Results obtained applying the cooling function (11) and (12) are shown in Table 4 and 5 respectively. The number of satisfied clauses, average time (minutes), and percentage of satisfied clauses are included in these tables. The mean percentage of satisfied clauses is 90.70% (with 1.81 minutes of executing time), and 89.4868 (with 0.1732 minutes) respectively. Whether only satisfiable instances are evaluated, these figures are 88.71% and 87.4269%.

# 6. CONCLUSIONS

SABBE algorithm is proposed in this paper. This algorithm can generate high quality solutions for SAT instances. The obtained results show that applying Boltzmann and Bose-Einstein distributions along with a Dynamical Equilibrium heuristic provide a good method for solving SAT instances. SABBE is a hybrid algorithm based on two acceptance distribution functions; these improve SA exploration capacity of solution space by exploiting bosons behavior at low temperatures, altering the acceptance probability of bad solutions in relation to system's temperature. In addition, the processing time required to find an optimal or near-optimal solution is reduced applying a tuning process over the SA parameters (i.e. number of Metropolis cycles) and the Dynamical Equilibrium heuristic. The processing cost required for these techniques is polynomial. Experimentation show that when simulated annealing is executed with both distribution functions at different temperature levels along with DEP, solutions quality is improve over the classical SA with only the Boltzmann distribution function.

<sup>&</sup>lt;sup>1</sup> SAT Competition, 2009. Satcompetition.Org. Available from http://www.satcompetition.org/2009.

-					14010 111150411000 105100						
#	Name	С	V	ρ	SA T	#	Name	С	V	ρ	SA T
1	sat-140-	336	140	2.	Y	19	unsat-109-100	228	109	2.09	Ν
	100			4							
2	sat-160-	384	160	2.	Y	20	unsat-115-100	244	115	2.12	N
-	100	201	100	4	-		unsur 110 100		110		1.
3	sat-180-	432	180	2.	Y	21	unsat-121-100	252	121	2.08	N
	100			4							
4	sat-200-	480	200	2.	Y	22	unsat-127-100	268	127	2.11	Ν
	100			4							
5	sat-220-	528	220	2.	Y	23	unsat-133-100	276	133	2.08	Ν
	100			4							
6	sat-230-	552	230	2.	Y	24	unsat-139-100	292	139	2.1	Ν
	100			4							
7	sat-240-	576	240	2.	Y	25	unsat-145-100	300	145	2.07	Ν
	100			4							
8	sat-250-	600	250	2.	Y	26	unsat-151-100	316	151	2.09	Ν
	100			4							
9	sat-260-	624	260	2.	Y	27	V360-c1530-	153	360	4.25	Y
	100			4			S144043535-002	0			
10	sat-270-	648	270	2.	Y	28	V360-c1530-	153	360	4.25	Y
	100			4			S368632549-051	0			
11	sat-280-	672	280	2.	Y	29	V360-c1530-	153	360	4.25	Y
	100			4			\$722433227-030	0			
12	sat-290-	696	290	2.	Y	30	V360-c1530-	153	360	4.25	Y
	100			4			S1293537826-039	0			
13	sat-300-	720	300	2.	Y	31	V360-c1530-	153	360	4.25	Y
	100			4			S1448866403-060	0			
14	unsat-61-	132	61	2.	Ν	32	V360-c1530-	153	360	4.25	Y
	100			16			S1459690542-033	0			
15	unsat-73-	156	73	2.	Ν	33	V360-c1530-	153	360	4.25	Y
	100			14			S1684547485-073	0			
16	unsat-85-	180	85	2.	Ν	34	34 V360-c1530-		360	4.25	Y
	100			12			S1711406314-093				
17	unsat-97-	204	97	2.	Ν	35	V360-c1530-	153	360	4.25	Y
	100			1			S1826927554-087	0			
18	unsat-	220	103	2.	Ν	36	V360-c1530-	153	360	4.25	Y
	103-100			14			S2032263657-035	0			

Table- 1.Instances tested

Table- 2.Initial and final temperatures for tested instances

#	$T_0 BP$	T <sub>0</sub> BEP	T <sub>f</sub> BEP	#	$T_0 BP$	T <sub>0</sub> BEP	T <sub>f</sub> BEP
1	8009.68	115.92	0.68	19	3741.17	50.99	0.68
2	8795.73	123.08	0.68	20	3847.3	56.72	0.68
3	9067.69	128.71	0.68	21	3870.52	59.01	0.68
4	9455.74	134.92	0.68	22	3960.07	56.15	0.68
5	9721.07	141.03	0.68	23	4132.53	58.72	0.68
6	10046.1	141.8	0.68	24	4119.27	60.73	0.68
7	10377.76	143.37	0.68	25	4251.93	59.3	0.68
8	10540.28	144.61	0.68	26	4311.63	62.16	0.68
9	10434.14	148.34	0.68	27	8626.58	116.3	0.68
10	11067.62	151.39	0.68	28	8799.04	134.35	0.68

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11	11100.79	158.84	0.68	29	8377.83	115.44	0.68
12	11190.34	158.89	0.68	30	8384.46	113.15	0.68
13	11405.92	154.35	0.68	31	8487.28	125.18	0.68
14	3081.16	42.11	0.68	32	8560.25	122.6	0.68
15	3240.36	46.41	0.68	33	8643.16	122.32	0.68
16	3419.45	49.27	0.68	34	8686.28	125.18	0.68
17	3618.45	52.14	0.68	35	8606.68	123.46	0.68
18	3638.35	52.42	0.68	36	8636.53	119.74	0.68

	<u> </u>		Cashing				1.		<u> </u>	
	Cooling		Coolin	g		Co	oling	(11)	Coolin	g (12)
	iuncuo	on (11)	iunctio	$\frac{n(12)}{2}$		IUI	nction	(11)	Tunctio	$\frac{n(12)}{2}$
Ħ	n	β	n	β	#	n		β	n	β
	value	value	value	value		val	lue	value	value	value
1	178.8 7	1.03	9.66	1.82	19	16	4.03	1.03	8.86	1.84
2	180.6 9	1.03	9.76	1.83	20	16	4.57	1.03	8.89	1.84
3	181.2 9	1.03	9.79	1.84	21	16	4.69	1.03	8.89	1.85
4	182.1	1.03	9.83	1.86	22	16	5.14	1.03	8.92	1.86
5	182.6 4	1.03	9.86	1.86	23	16	5.97	1.03	8.96	1.86
6	183.2 8	1.03	9.9	1.87	24	16	5.9	1.03	8.96	1.87
7	183.9 2	1.03	9.93	1.87	25	16	6.52	1.03	8.99	1.88
8	184.2 2	1.03	9.95	1.76	26	16	6.79	1.03	9.01	1.89
9	184.0 2	1.03	9.94	1.88	27	18	0.31	1.04	9.74	1.97
10	185.1 7	1.03	10	1.88	28	18	0.7	1.04	9.76	1.96
11	185.2 3	1.03	10	1.88	29	17	9.74	1.04	9.7	1.97
12	185.3 9	1.03	10.01	1.89	30	17	9.76	1.04	9.71	1.97
13	185.7 6	1.04	10.03	1.89	31	18	0.71	1.04	9.76	1.96
14	160.2 4	1.03	8.65	1.74	32	18	0.16	1.04	9.73	1.97
15	161.2 3	1.03	8.71	1.77	33	18	0.35	1.04	9.74	1.97
16	162.2 7	1.03	8.76	1.8	34	18	0.45	1.04	9.74	1.96
17	163.3 8	1.03	8.82	1.82	35	18	0.27	1.04	9.73	1.97
18	163.4 8	1.03	8.83	1.83	36	18	0.34	1.04	9.74	1.97

**Table- 3.**n and  $\beta$  parameters for every tested instance

#	Satisfied	Average	%	#	Satisfied	Average	%
	Clauses	Time	Satisfied		Clauses	Time	Satisfied
	Chudbes	(minutes)	Clauses		Chudses	(minutes)	Clauses
1	299.87	0.58	89.25	19	214.87	0.24	94.24
2	339.93	0.74	88.52	20	229.33	0.27	93.99
3	381.13	0.91	88.22	21	236.43	0.28	93.82
4	421.5	1.07	87.81	22	251.37	0.32	93.79
5	461.33	1.32	87.37	23	258.93	0.33	93.82
6	481.67	1.45	87.26	24	273.73	0.37	93.74
7	501.6	1.5	87.08	25	281.17	0.4	93.72
8	521.63	1.66	86.94	26	295.43	0.45	93.49
9	542.57	1.8	86.95	27	1383.9	4.27	90.45
10	560.7	1.97	86.53	28	1385.33	4.23	90.54
11	581.1	2.04	86.47	29	1383.5	4.19	90.42
12	601.9	2.2	86.48	30	1383.93	4.19	90.45
13	622.47	2.28	86.45	31	1382.37	4.13	90.35
14	125.93	0.09	95.4	32	1385.97	4.17	90.59
15	148.27	0.12	95.04	33	1386.47	4.28	90.62
16	170.77	0.16	94.87	34	1384.4	4.25	90.48
17	192.7	0.2	94.46	35	1386.17	4.28	90.6
18	207.50	0.24	94.32	36	1385.90	4.26	90.58

Table- 4. Results of SABBE with cooling function (11)

**Table- 5.**Results of SABBE with cooling function (12)

#	Satisfied Clauses	Average Time (minutes)	% Satisfied Clauses	#	Satisfied Clauses	Average Time (minutes)	% Satisfied Clauses
1	292.87	0.05	87.16	19	212.47	0.02	93.19
2	331.73	0.08	86.39	20	226.37	0.03	92.77
3	371.93	0.06	86.09	21	234.4	0.03	93.02
4	411.53	0.09	85.74	22	248.83	0.03	92.85
5	450.97	0.11	85.41	23	255.7	0.03	92.64
6	470.47	0.11	85.23	24	269.87	0.04	92.42
7	491.5	0.13	85.33	25	277.1	0.03	92.37
8	512.57	0.16	85.43	26	292.63	0.06	92.6
9	532.9	0.17	85.4	27	1373.93	0.39	89.8
10	550.47	0.17	84.95	28	1373.4	0.4	89.76
11	570.93	0.21	84.96	29	1375.9	0.4	89.93
12	590.4	0.23	84.83	30	1374.37	0.35	89.83
13	614.6	0.36	85.36	31	1374.2	0.38	89.82
14	124.83	0.01	94.57	32	1374.77	0.47	89.85
15	146.97	0.01	94.21	33	1375.87	0.38	89.93
16	168.17	0.01	93.43	34	1376.17	0.42	89.95
17	190.37	0.01	93.32	35	1374.90	0.43	89.86
18	205.30	0.02	93.32	36	1374.13	0.37	89.81

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Instanc	Satisfied	Average Time	% Satisfied	Instance	Satisfied	Average Time	% Satisfied
C	Clauses	(minutes)	Clauses		Clauses	(minutes)	Clauses
1	298.4	0.44	88.81	19	214.83	0.19	94.22
2	338.57	0.57	88.17	20	229.37	0.21	94
3	379.57	0.71	87.86	21	236.67	0.22	93.92
4	420.93	0.86	87.69	22	251.03	0.25	93.67
5	461.5	1.01	87.41	23	258.73	0.25	93.74
6	481.8	1.11	87.28	24	273.43	0.28	93.64
7	500.57	1.18	86.9	25	280.5	0.3	93.5
8	519.83	1.3	86.64	26	295.03	0.33	93.36
9	541.73	1.39	86.82	27	1383.03	3.28	90.39
10	559.63	1.5	86.36	28	1383.83	3.24	90.45
11	581.47	1.59	86.53	29	1383.8	3.22	90.44
12	601.07	1.69	86.36	30	1384.43	3.21	90.49
13	620.6	1.77	86.19	31	1382.7	3.26	90.37
14	125.83	0.07	95.33	32	1383.63	3.3	90.43
15	148.37	0.1	95.11	33	1383.2	3.28	90.41
16	170.4	0.12	94.67	34	1383.37	3.27	90.42
17	192.13	0.15	94.18	35	1383.9	3.27	90.45
18	207.23	0.17	94.2	36	1383.43	3.28	90.42

Table- 6. Results of Classical Simulated Annealing with cooling function (11)

Table- 7. Results of Classical Simulated Annealing with cooling function (12)

Instance	Satisfied	Average	%	Instance	Satisfied	Average	%
	Clauses	Time	Satisfied		Clauses	Time	Satisfied
		(minutes)	Clauses			(minutes)	Clauses
1	289.1	0.02	86.04	19	211.93	0.01	92.95
2	328.13	0.03	85.45	20	226.4	0.01	92.79
3	369.3	0.03	85.49	21	233.13	0.01	92.51
4	411.17	0.06	85.66	22	247.47	0.02	92.34
5	447.8	0.07	84.81	23	254.4	0.02	92.17
6	466.03	0.07	84.43	24	269.3	0.02	92.23
7	486.63	0.08	84.48	25	276.13	0.02	92.04
8	505.07	0.08	84.18	26	290.57	0.03	91.95
9	525.97	0.09	84.29	27	1369.7	0.16	89.52
10	546.93	0.09	84.4	28	1370.57	0.16	89.58
11	565.8	0.12	84.2	29	1369	0.16	89.48
12	587.63	0.13	84.43	30	1367.5	0.16	89.38
13	606	0.14	84.17	31	1367.47	0.16	89.38
14	123.87	0	93.84	32	1368	0.16	89.41
15	145.3	0.01	93.14	33	1368.93	0.16	89.47
16	167	0.01	92.78	34	1369.1	0.16	89.48
17	189.37	0.01	92.83	35	1370.67	0.16	89.59
18	203.87	0.01	92.67	36	1370.70	0.16	89.59

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